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# **Efficient Catalytic Hydrocracking of Crude Palm Oil Over EDTA Template-assisted SiO2-Al2O3/NiMo Catalysts**

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#### **Abstract**

The development of hydrocracking catalysts for crude palm oil (CPO) is a challenging process due to its limited textural or pore accessibility and low acidity properties. Therefore, this study aims to develop a series of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo catalysts using different Al mass (*x* = 5, 10, 25 g) assisted with EDTA to enhance their physicochemical properties. During the procedures, bimetallic NiMo species were dispersed into SiO<sub>3</sub>-Al<sub>2</sub>O<sub>3</sub>-x using the wet impregnation method. The structural, textural, surface morphology, particle size distribution, and acidity properties of the products were then assessed. Catalytic activity of catalysts on hydrocracking of CPO was evaluated at 350 °C for 2 h, H<sub>2</sub> gas pressure of 20 bar, and mixed at 1500 rpm. The results showed that increasing Al mass caused an increment in the total acidity, acid site density, and surface area of SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-x. In addition, SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-25 provided better support properties, allowing preferable NiMo dispersion. Hydrocracking assessment showed that CPO conversion was increased at higher Al mass, producing the highest bio-aviation and biogasoline fractions yield. Based on these results, SiO<sub>3</sub>-Al<sub>2</sub>O<sub>3</sub>-x/NiMo successfully enhanced CPO conversion of unloaded SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-x, as well as increased the yield of bio-aviation and biogasoline fractions.

#### **Keywords**

catalytic hydrocracking, NiMo, SiO<sub>2</sub>-Al<sub>2</sub>O<sub>2</sub>, crude palm oil, bimetallic catalyst

#### **1 Introduction**

The growing need for energy and the decreasing supply of conventional fuel are major factors facilitating the development of cleaner and sustainable energy [1]. Consequently, biofuel production from renewable resources has received significant attention in recent years. This is primarily due to its ability to compensate for the decreasing supply of fossil fuels, lower carbon footprint, as well as enhance economic growth and sustainability [2]. Biofuel production is often carried out using crude palm oil (CPO) and its derivatives as biomass due to their low cost and high output per hectare relative to other vegetable oils in Southeast Asia [3]. At present, the most prevalent method for this process is triglyceride hydroprocessing, which comprises the use of high temperature and pressure with different catalysts [4]. Triglyceride hydroprocessing typically consists

of several steps, including hydrogenation and cracking. Hydrogenation often begins by transforming unsaturated fatty acids into saturated acids, followed by breaking fatty acids into short-chain hydrocarbons through complex chemical processes, such as hydrodeoxygenation, decarboxylation, and decarboxylation [5]. Meanwhile, hydrocracking converts CPO into hydrocarbons, which is an alternate method for producing low S and N hydrocarbons.

Several studies have shown that the types of catalysts significantly impact the efficiency of hydrocracking. Various types, such as HZSM-5 and HY zeolites [6], Zn-Mo/HZSM-5 [7], Ni/zeolite [8], ZSM5 zeolite [9],  $Mo/SiO<sub>2</sub>$  [10],  $SiO<sub>2</sub>/ZrN$  [11], NiO-CdO/biochar [12], Ni-Mo/alumina [13], Ni–W/SiO<sub>2</sub>–Al<sub>2</sub>O<sub>3</sub> [14], and NiMoW-ZSM-5/MCM-41 [15], have been used for vegetable

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oil-based hydrocracking. Despite the potential, noble monometal-based catalysts are less effective due to the ease of deactivation by sintering active metal species and coke deposits, leading to unstable and poor catalytic activity [16]. This has led to the use of bifunctional catalysts, which often comprise both metal and acid sites. The materials also have hydrogenation sites that can supply hydrogen for hydrogenation processes and surface hydrogenolysis [17]. Although noble metal-based catalysts perform better in hydrocracking, their high costs can diminish economic viability, necessitating the consideration of alternatives [16]. Among the transition metals, Ni and Mo are commonly used in hydrocracking reactions and have shown exceptional catalytic activity [18].

Various types of catalysts using NiMo as active metals have been prepared with different supports [19–24]. In this context, alumina and silica are the most frequently used mesoporous oxide supports due to their tunable acidity and excellent stability [25, 26].  $SiO_2$ - $Al_2O_3$  mixed oxides are prominent supports that offer various benefits during hydrocracking process. This material has adequate pore diameter to promote metal deposition and pore diffusion, optimal active metal dispersion, and appropriate acidity to break down larger molecules while reducing coke formation.  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub> oxides can also be modified to provide the desired acidity and textural characteristics [27, 28]. According to a previous study [11], the use of ethylenediaminetetraacetic acid (EDTA) as a template method successfully enhanced the acidity, metal dispersion, and textural features of SiO<sub>2</sub>/Zr-based catalysts, providing better catalytic hydrocracking performance. Therefore, this study aims to develop mesoporous  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>/NiMo catalysts with different Al mass using EDTA as a template agent to enhance their physicochemical properties. Dispersing NiMo into  $SiO_2$ - $Al_2O_3$  supports is expected to enhance the intrinsic performance of CPO hydrocracking towards high conversion.

### **2 Materials and methods**

## $2.1$  Preparation of  $\text{SiO}_2\text{-} \text{Al}_2\text{O}_3$

 $SiO_2$ -Al<sub>2</sub>O<sub>3</sub> was prepared using the sol-gel method with different Al mass (5, 10, 25 g with Si:Al ratio 1:0.02, 1:0.05, 1:0.15, respectively) and assisted with EDTA as a template. All chemicals for catalyst preparation were purchased from Sigma-Aldrich and used without further purification. A total of 25 g of disodium salt of EDTA  $(C_{10}H_{14}N_2Na_2O_8.2H_2O, 99.0–101.0%$  purity) was dissolved in demineralized water (500 mL) and stirred, thus

forming 5% of EDTA solution. Subsequently, 5 g of aluminum nitrate nonahydrate salts  $(AI(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O, \geq 98.5\%$ purity) were dissolved in 100 mL of as-prepared EDTA solution and stirred at room temperature, and were later mixed with 100 mL of tetraethyl orthosilicate  $(Si(OC<sub>2</sub>H<sub>5</sub>)<sub>4</sub>$ ,  $\geq$ 99.0%) and 200 mL of ethanol (CH<sub>3</sub>OH,  $\geq$ 99.5 purity) and stirred for 15 min at room temperature. Furthermore, the ammonia solution (NH<sub>4</sub>OH, 25% purity) was gradually dripped into the latter solution until it became a gel, which was agitated for 30 min and subsequently stirred and heated up to 50 °C until forming a paste. The paste was dried at 100 °C for 24 h and calcined at 750 °C for 6 h. Its powder (120 mesh) was denoted as  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5. Further catalysts with different Al mass (10 and 25 g) was prepared with the same procedures and were denoted as  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10 and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25, respectively.

# **2.2 Preparation of SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>/NiMo**

 $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>/NiMo was prepared using the wet-impregnation method. Typically, 5.06 g of nickel(II) chloride hexahydrate salt (NiCl<sub>2</sub>⋅6H<sub>2</sub>O, 99.9% purity) was dissolved in 100 mL of demineralized water and stirred at room temperature. A total of 5.26 g of ammonium molybdate  $((NH_4)$ <sub>2</sub>MoO<sub>4</sub>, purity 99.98%) was dissolved in 100 mL of demineralized water and mixed with the latter solution, forming NiMo precursors solution (molar ratio = 1:1). Furthermore, 25 g of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub> was dispersed in the NiMo solution and stirred, gradually increasing the temperature to 80 °C until forming a paste, which was dried in the oven at  $100-110$  °C, calcined at 750 °C for 6 h, and at 350 °C for 2 h. The powder was denoted as  $SiO_2$ - $Al_2O_3$ -x/ NiMo, where x was the mass of Al.

#### **2.3 Hydrocracking of CPO**

In this procedure, 0.6 g of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/ NiMo series catalysts and 20 g of CPO were used for hydrocracking and before hydrocracking, the reactor was purged 3 times with  $H_2$  gas (20 bar). Hydrocracking was conducted at 350 °C for 2 h uder stirring with 1500 rpm. The liquid product was analyzed by the GC-MS. The triglycerides were denoted as TGs, whereas the biofuel yield  $(Y_x)$  and conversion  $(C_x)$  were calculated according to Eqs.  $((1)–(2))$ :

$$
Y_x = \frac{\% \text{ area of biofuel in GC-MS}}{\text{TGs in reactant} - \text{TGs in product}} \times 100\%,\tag{1}
$$

$$
C_x = \frac{\text{TGs in reactant} - \text{TGs in product}}{\text{TGs in reactant}} \times 100\%.\tag{2}
$$

#### **2.4 Characterization of catalysts**

Powder X-ray diffraction (XRD, Rigaku SmartLab) was used to analyze the phase structure of the catalysts, and FTIR spectrophotometer (Bruker Tensor II) was used to evaluate the functional groups of the catalysts. SEM-EDX mapping (Hitachi SU3500) was used to capture the surface morphology of the catalysts and their elemental constituents. The average particle size and its distribution were calculated on a micro-scale using a particle size analyzer (Horiba LA-960). Furthermore, the  $N_2$  adsorption-desorption was recorded by a surface area analyzer (TriStar II 3020 , Micromeritics). The sample (0.3 g) was degassed at 300 °C for 3 h, with bath temperature of −195.85 °C and equilibration Interval of 5 s. The weight of the degassed sample was utilized in calculations.

 The surface area was calculated using the multi-point Brunauer–Emmett–Teller method (BET), while the pore features were extracted using Barrett-Joyner-Halenda (BJH) method. The total acidity was measured using an NH<sub>3</sub>-TPD (AutoChem II 2920, Micromeritics). The sample was degassed at 350 °C for 1 h and flowed with He gas. Subsequently, the temperature was increased gradually up to 500 °C for 30 min.

#### **3 Results and discussion**

#### **3.1 Catalyst characterization**

The XRD diffractograms of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ - $Al_2O_3$ -x/NiMo where x is the mass of Al (5, 10, 25 g) were presented in Fig. 1. The parent  $SiO_2$ - $Al_2O_3$ -5 showed a wide diffraction peak at 2θ ca. 21°, suggesting the formation of amorphous silica structure [29]. The diffraction peaks appeared at  $2\theta = 27.46^{\circ}$ , 31.17°, 35.85°, and 46.82°, confirming the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> phase [30]. The broadened peak ( $2\theta = 21^\circ$ ) upon higher Al mass ( $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10



**Fig. 1** XRD diffractograms of parent  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub> and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>/NiMo catalysts with different Al masses

and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25) showed a robust interaction between SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> [31]. The intensity of the *γ*-Al<sub>2</sub>O<sub>3</sub> phase in  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10 significantly decreased and tended to disappear in  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25, implying that higher mass of Al decreased the crystallinity and promoted the formation of amorphous  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub> support. The  $\text{SiO}_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo catalyst exhibited a diffraction peak at 2θ 14.27°, 23.98°, 25.32°, 28.24°, 32.60°, and 48.32° corresponding to the presence of crystalline  $MoO<sub>2</sub>[32]$ . The monoclinic phase of the nickel molybdenum could be confirmed by the diffraction peaks at 2θ 25.97°, 26.77°, 27.4°, and 32.87° [33], while the diffraction peaks at 2θ 38.69°, 43.85°, and 61.75° were attributed to the nickel oxide phase [34]. The intensity of sharp peaks of metallic phases was much higher in the order of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo >  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10/  $NiMo > SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-25/NiMo$  catalysts, which showed the presence of larger NiMo crystallite and poor dispersion in the support [35]. This result suggested that  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25 promoted better the bimetal dispersion than its counterparts. However, the diffraction intensity of silica  $(SiO_2-Al_2O_3-5$ NiMo) increased upon NiMo loading owing to the interaction of the bimetallic species with the silica, which influenced the regularity of the  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub> framework.

Fig. 2 presented FTIR spectra of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo. The absorption bands at 805 cm<sup>-1</sup> and  $1066-1198$  cm<sup>-1</sup> in SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-5 corresponded to the linkage vibration of Si-O-Al and the stretching vibration of Si-O-Si of the condensed silica-alumina framework formation, respectively [11, 36], and indeed had similar absorption bands characteristics to its counterparts. However, the shift upon higher Al mass in the silica bond



**Fig. 2** FTIR spectra of parent  $SiO_2$ - $Al_2O_3$  and  $SiO_2$ - $Al_2O_3/NiMo$ catalysts with different Al masses

 $(SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-10$  and  $SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-25)$  presumably showed the increase of Si–O–Al hetero-linkages population in catalysts [37]. The absorption bands at  $620-703$  cm<sup>-1</sup> in  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo were ascribed to the Mo–O–Mo and Mo=O vibrations [22], while the absorption bands at 932–962  $cm^{-1}$  were attributed to the Ni-O vibration. Similar absorption bands were also observed in  $SiO_2$ - $Al_2O_3$ -10/NiMo with no appreciable changes. These absorption bands of the metals, however, tended to diminish in  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25/NiMo, suggesting a better interaction between the bimetallic species and the support, which was consistent with the XRD results. Moreover, the Si-O-Al absorption band in  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo were slightly shifted to lower wavenumbers (ca.  $795 \text{ cm}^{-1}$ ) and had higher intensity with respect to the parent catalysts, suggesting that the bimetalic species were incorporated into the framework of catalysts support [29].

Fig. 3 showed the SEM micrographs of unloaded  $SiO_2$ - $\text{Al}_2\text{O}_3$ -x and SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-x/NiMo. SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-5 (Fig. 3 (a)) exhibited aggregated particles with irregular shapes, suggesting an amorphous nature [38]. Similar surface morphology features were also noticed in both  $SiO_2Al_2O_3$ -10 and  $SiO_2Al_2O_3$ -25 (Fig. 3 (b)–(c)). A change in surface morphology features was observed upon NiMo loading (Fig. 3 (d)–(f)), showing that changing the Al mass in the support could affect the surface morphology of the  $\rm SiO_{2}$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo catalysts. Different Al mass in the support presumably reorganizes the arrangement of the particles within the surface, hence resulting in different morphologies upon NiMo loading.

Fig. 4 presented the EDX mapping of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo.  $SiO_2$ -SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-5 (Fig. 4 (a)) showed Si and Al elements, confirming the formation of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>, which was similar to  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10 and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25 (Fig. 4 (b)–(c)) with increasing Al elements intensity upon higher Al mass. Ni and Mo element with homogenous distribution



**Fig. 3** SEM micrographs of (a)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5; (b)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10; (c)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25; (d)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo; (e)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo; (f)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo



**Fig. 4** SEM-EDX mapping of (a)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5; (b)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10; (c)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25; (d)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo; (e)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo; (f)  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo

appeared in  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo (Fig. 4 (d)–(f)), showing that the NiMo species were successfully loaded onto the support. Fig. 4 showed that  $SiO_2$ - $Al_2O_3$ -25/NiMo had more profound Ni and Mo intensity compared to its counterparts, suggesting an enhancement in the bimetal dispersion, corroborating the XRD and FTIR results.

The particle size distribution of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo was presented in Fig. 5, while the average particle size of catalysts was shown in Table 1.  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5 had a narrow particle size distribution with an average particle size of  $5.63 \pm 0.02$  µm. This size



**Fig. 5** The particle size distribution of  $SiO_2$ - $Al_2O_3$ -x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo catalysts

**Table 1** The average particle size of  $SiO_2$ - $Al_2O_3$ -x and of

$SiO_{2}$ -Al <sub>2</sub> O <sub>2</sub> -x/NiMo catalysts			
Catalysts	Average particle size $(\mu m)$		
$SiO_{2}$ -Al <sub>2</sub> O <sub>3</sub> -5	$5.63 \pm 0.02$		
$SiO, -Al, O, -10$	$16.88 \pm 0.06$		
$SiO, -Al, O, -25$	$9.78 \pm 0.02$		
$SiO, -Al, O, -5/NiMo$	$7.48 \pm 0.02$		
$SiO, -Al, O, -10/NiMo$	$5.45 \pm 0.02$		
$SiO, -Al, O, -25/NiMo$	$6.26 \pm 0.02$		

distribution became wider with increasing average particle size  $16.88 \pm 0.06$  µm in SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-10, suggesting a non-uniform particle size distribution. The particle size distribution tended to narrow upon higher Al mass  $(SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-25)$ and to decrease its average particle size to  $9.78 \pm 0.02$  µm.  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo showed a higher average particle size  $(7.48 \pm 0.02 \mu m)$  that slightly shifted towards higher particle diameter distribution for its parent catalysts, presumably owing to NiMo agglomeration. Meanwhile,  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10/ NiMo and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25/NiMo had narrow particle size distribution and a decrease in the average particle size  $(5.45 \pm 0.02$  and  $6.26 \pm 0.02$  µm, respectively) compared to unloaded  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>, showing that increasing the Al weights prominently promoted better homogeneity of the particles hence providing good dispersion.

Fig. 6 showed the  $N_2$  adsorption-desorption of isotherms  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo. However, it appeared that all catalysts possessed type IV isotherm, showing mesoporous materials [39]. The presence of mesopores allowed an efficient movement of large molecules through the pores. The steep capillary condensation in the



**Fig. 6** N<sub>2</sub> adsorption-desorption of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/ NiMo with different Al mass

relative pressure  $P/P_0$  range of 0.65–0.85 was attributed to the non-uniform pore sizes and shapes [40].

Table 2 showed the BET surface area, pore volume, and the average pore diameter (which was calculated with the BJH method) of prepared catalysts. In addition, it could be seen that  $SiO_2$ - $Al_2O_3$ -10 had a higher surface area than  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5 as well as pore volume and tended to increase upon higher weights of Al. This result could be attributed to the pore enlargement by Si-O-Al bonding [41]. However, upon NiMo loading, the surface area tended to decrease significantly in both  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10/ NiMo. This happened presumably owing to the partial occupation or blockage of the pore space in the support of the active metal phase [42, 43].  $SiO_2$ - $Al_2O_3$ -25/NiMo possessed the highest surface area than its counterpart and increased pore diameter for the unloaded  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25. The reason presumably could be due to changes in the electrostatic field in the pores of the support as the Al mass increases, which could cause electrostatic equilibrium in the pore supports, leading to an increase in pore diameter.

The total acidity of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/ NiMo catalysts measured by  $NH<sub>3</sub>$ -TPD was presented in Table 3 and the total acidity of unloaded  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x showed no appreciable change (~0.53 mmol NH<sub>3</sub> g<sup>-1</sup> cat.) with increasing Al mass. The total acidity value

**Table 2** The textural features of  $SiO_2$ - $Al_2O_3$ -x and  $SiO_2$ - $Al_2O_3$ -x/NiMo

catalysts					
Catalysts	<b>BET</b> surface area $(m^2 g^{-1})$	Pore volume $\rm (cm^3 \ g^{-1})$	Average pore diameter (nm)		
$SiO, -Al, O, -5$	59	0.29	19.56		
$SiO, -Al, O, -10$	240	0.91	15.07		
$SiO, -Al, O, -25$	326	1.26	15.38		
$SiO_{2}$ -Al <sub>2</sub> O <sub>3</sub> -5/ NiMo	$\mathfrak{D}$	0.004	8.66		
$SiO, -Al, O, -10/$ <b>NiMo</b>	$\mathfrak{D}$	0.004	7.93		
$SiO, -Al, O, -25/$ NiMo	64	0.33	20.38		

**Table 3** Total acidity of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo catalysts measured by  $NH<sub>3</sub>$ -TPD



was predominantly driven by Lewis and Bronsted acid sites from silica and alumina, which tended to double upon higher Al mass  $(SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-25)$  up to 1.07 mmol NH<sub>3</sub> g<sup>-1</sup> cat. due to the enhancement of  $Al^{3+}$  Lewis acid sites. Meanwhile, a decrease in total acidity was noticed in  $\rm SiO_{2}$ -Al<sub>2</sub>O<sub>3</sub>-x upon NiMo loading. This result was presumably due to the aggloeration of the NiMo species, which led to the blocking of the alumina-silica acidic sites [44]. Compared to its counterparts, the total acidity increased in the order of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo >  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10/NiMo  $>$  SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-25/NiMo. However, this seemed to have a linear correlation with the surface area, suggesting that a high surface area could lead to high total acidity.

Fig. 7 showed  $NH_3$ -TPD profiles of unloaded  $SiO_2$ - $Al_2O_3$ -x and  $SiO_2$ - $Al_2O_3$ -x/NiMo with different Al mass. The desorption peaks at  $\leq 200$  °C, corresponded to weak acidic sites, while the desorption peaks at 200–300 °C and  $>$  300 °C showed the presence of medium and strong acidic sites, respectively [20].  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5 had only strong acidic sites, while  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10 had both weak and strong acidic sites. The desorption peak intensity tended to increase pronouncedly upon higher Al mass  $(SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-25)$ ,



Fig. 7 NH<sub>3</sub>-TPD profiles of SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-x and SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-x/NiMo with<br>
SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-x possessed a higher yield of biogasoline upon -TPD profiles of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo with different Al mass

suggesting that increasing the Al mass led to an increase in the density of acidic and formed weak acidic sites. Both  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/NiMo and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-10/NiMo had only strong acidic sites, but the latter had lower acid density. Moreover,  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25/NiMo had weak and strong acidic sites with higher density, showing better acidity strength compared to its counterparts.

#### **3.2 Catalytic performance in CPO hydrocracking**

Table 4 shows the catalytic performance of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiM in terms of CPO conversion and biofuel yield. Additionally, it could be seen that  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5 had the lowest CPO conversion (75.78%) and tended to rise to 84.47% upon introducing 10 g Al on the support  $(SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-10)$ . The highest CPO conversion up to 91.20% was achieved by  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-25, showing that increasing Al mass promoted higher CPO conversion owing to the weak-strong acidic sites derived from Si–(OH)–Al. It was reported that hydrocracking performance increased with the increase in the acidity of the catalyst [45]. Upon NiMo loading,  $SiO_2/Al_2O_3 - 5$  had higher CPO conversion (92.99%) than its parent catalyst, presumably due to the moderately dispersed active metal within the pores of the catalyst, hence increasing its catalytic activity. Similarly,  $SiO_2/Al_2O_3$ -10 showed higher CPO conversion (91.34%) as well as  $SiO_2/Al_2O_3-25/NiMo$  (91.73%), suggesting a synergetic effect between the former acidic sites from alumina-silica and the dispersed NiMo species onto the support hence enhancing the CPO conversion. Although no appreciable change in the CPO conversion  $(\sim)91-92\%)$  was noticed in the case of the NiMo catalyst analogues, however, it possessed different catalytic activity in terms of biofuel yields.  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5 exhibited predominant bio-aviation (34.26%), followed by biodiesel (2.28%), and had the lowest biogasoline yields (2.28%). The high bio-aviation yield was attributed to the mesoporous structure that provided better diffusion and accessibility between the CPO and acidic sites, hence selectively forming  $C_{10}-C_{14}$  carbons. Unloaded

**Table 4** Catalytic activity of  $\text{SiO}_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $\text{SiO}_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo towards hydrocracking of CPO

Catalysts		Yield $(\% )$		
	Conversion $(\% )$	Biogasoline $(C_s - C_o)$	Bio-aviation $(C_{10} - C_{14})$	Biodiesel $(C_{15} - C_{22})$
$SiO_{2}$ -Al <sub>2</sub> O <sub>3</sub> -5	75.78	2.28	34.26	17.22
$SiO_{2}$ -Al <sub>2</sub> O <sub>3</sub> -10	84.47	2.85	44.55	8.58
$SiO_{2}$ -Al <sub>2</sub> O <sub>3</sub> -25	91.20	11.15	46.31	11.76
$SiO_{2}$ -Al <sub>2</sub> O <sub>3</sub> -5/NiMo	92.99	18.13	62.92	1.70
$SiO_{2}$ -Al <sub>2</sub> O <sub>3</sub> -10/NiMo	91.34	13.26	61.31	2.34
$SiO2-Al2O2-25/NiMo$	91.73	18.47	58.00	2.00

introducing higher Al mass onto the support, presumably owing to the higher surface area and dominantly small pore diameter. It was reported that the fraction of gasoline was much more favorable to diffuse into a small pore than the larger fractions [16]. Upon NiMo loading,  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-5/ NiMo showed an increase in bio-aviation yield up to 62.92% along with higher biogasoline and decreased biodiesel yield compared to the unloaded  $SiO_2$ - $Al_2O_3$ , which suppressed the formation of longer carbon chain biofuel due to the excessive cracking of longer carbon towards shorter carbon chain biofuels. The same trends were also observed with  $SiO_2$ - $Al_2O_3$ -10/NiMo and  $SiO_2$ - $Al_2O_3$ -10/NiMo with comparable catalytic activity for unloaded  $SiO_2$ - $Al_2O_3$ -x, showing that  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo promoted higher CPO yield and shortchain biofuels yield. Compared to  $SiO_2/Zr$ -KHF and  $SiO_2/$ ZrN-EDTA prepared by the template approach, the present catalysts showed comparable results with their counterparts under lower hydrocracking temperatures [11, 43]. Despite that controlling the Al mass in  $SiO_2/Al_2O_3$ -NiMo showed the textural and acidity features dependency. Future studies however must address the composition of the different phases and their oxidation state to completely understand the inherent features that eventually affect catalytic activity.

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#### **4 Conclusion**

The effect of Al mass on the structure, acidity features, and CPO hydrocracking catalytic performance of  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x and  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x/NiMo were presented. Increasing Al mass led to an increase in the total acidity, surface area, and the amorphous feature of  $SiO_2/Al_2O_3$ .  $SiO_2/Al_2O_3$ -25 exhibited a better support, as evidenced by providing well-dispersed NiMo species. Hydrocracking test of the CPO showed that  $SiO_2$ - $Al_2O_3$ -x/NiMo had higher CPO conversion and successfully formed higher dominant bio-aviation and biogasoline yields compared to unloaded  $SiO_2$ -Al<sub>2</sub>O<sub>3</sub>-x. These catalysts successfully suppressed the long carbon chain favoring the short carbon chain, showing good hydrocracking activity. Further analysis regarding the composition of different phases and their oxidation state must be considered to comprehend the properties of the catalysts and their catalytic process in CPO conversion.

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