Optimisation of Microwave Pretreatment for Biogas Enhancement through Anaerobic Digestion of Microalgal Biomass

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Abstract

In this study, optimization of microwave (MW) pretreatment conditions for anaerobic digestion of green microalgae (Enteromorpha) is carried out by using response surface methodology (RSM). MW power, pretreatment time and liquid-solid ratio were selected as independent variables for optimization. The optimum conditions were achieved at MW power, pretreatment time and liquid-solid ratio of 656.92 W, 5.10 min and 33.63:1, respectively. From these optimum conditions, it was found that MW pretreatment power of about 600 W had better effect. An anaerobic digestion was carried out batch-wise with working volume, operating temperature and mixing rate as 250 ml, 37 °C and 150 rpm, respectively. Optimum conditions provide highest amount of COD and reducing sugar increase of 10,420 mg/L and 0.77-0.79 g/L respectively. The increase in COD and reducing sugar showed that the pretreatment has improved anaerobic digestion of microalgae. The peak biogas production amount of MW pretreated 20:1, 6 min group reached 244 mL whereas the control group only reached 188 mL in total.

Keywords

anaerobic digestion, biofuel, biomass, microwave (MW) pretreatment, response surface methodology

1 Introduction

Today's society is highly dependent on fossil fuels such as crude oil, natural gas, lignite and coal [1]. These natural reserves are region specific and may cause depletion of resources in some regions after a certain amount of time. Our industrialized society is highly dependent on the use of energy sources for the continuation of its economic and welfare growth. Biomass is a renewable energy source, which has the potential to provide high energy fuel for heating, cooling and electrical purposes in its all three forms (solid, liquid and gas) [2]. Biogas is produced due to bio-decomposition of organic material caused by bacteria in anaerobic conditions. Instant storage and usage as a substitute of natural gas is the primary advantage of biogas [3]. To encounter the growing demands of energy across the world and waste disposal, production and distribution of biogas from organic matter could serve as one possible solution.

Anaerobic digestion is a biochemical and microbiological process in which decomposition of organic matter takes place in the absence of oxygen [4]. The anaerobic digestion process consists of four main conversion phases of organic matter into biogas namely; hydrolysis, acidogenesis, acetogenesis and methanogenesis [5]. In the first phase large and complex organic matter such as carbohydrates, fats and proteins react with water to form monomers by the assistance of hydrolytic bacteria. During the second phase conversion of monomers into volatile fatty acids (VFAs) is carried out by the aid of fermentative bacteria. The third phase involves the transformation of VFA into acetic acid, carbon dioxide (CO_2) and hydrogen under the action of acetogenic bacteria. During the final phase, methanogenic bacteria convert acetic acid and hydrogen into methane (CH_4) and CO_2 [6]. The stages of anaerobic digestion process are shown in Fig. 1.

Hydrogen production via fermentative biomass has more advantage over the traditional hydrogen preparation methods as it does not require an abundance of chemical raw materials, in addition the production process does not require consuming a lot of energy. Biological hydrogen production is better than other traditional methods of production as it is green [7]. Aquatic algal biomass, which can be sourced from natural algal bloom or mass cultivation, is considered as a
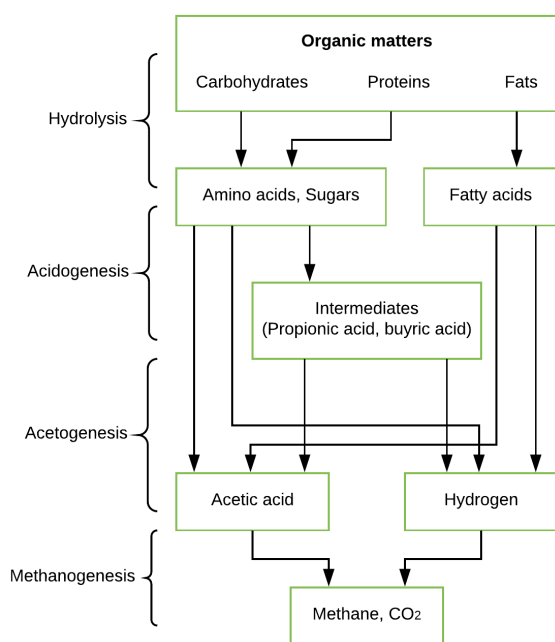
Fig. 1 Stages of anaerobic digestion process

promising substrate for hydrogen fermentation [8]. Previous studies indicated that anaerobic sludge (AS) and microalgae were co-cultured to enhance the energy conversion and nutrients removal from starch waste water [9].

Hydrolysis is considered as the rate limiting step in anaerobic digestion process. Pretreatment techniques have been used to improve hydrolysis and anaerobic digestion performance [10]. Numerous pretreatment techniques have been instigated for complex substrates, such as mechanical, thermal, chemical or biological treatments [11]. Microwave (MW) pretreatment is a thermal pretreatment method, which can obtain the desired temperature faster than conventional heating methods and the process is energy efficient too. The optimization of MW pretreatment conditions is very important in order to get an energy efficient overall improvement on fermentation conditions.

The RSM is a useful tool for improving and optimizing unknown systems or processes in combination with mathematical methods and statistical analysis [12]. In this method, an experimental design is used to effectively respond on the surface design and the statistical model of the information by establishing a fitting curve which is obtained when the experimental design is applied. The scientific map describes the relationship between the response and the variable.

The aim of the present study is to explore the effect of MW pretreatment on the anaerobic digestion of green algae (*Enteromorpha*). RSM is used for finding the optimum condition for the multivariate interactive factors for this method of pretreatment. To understand the effectiveness of the MW pretreatment, measurements of soluble indexes including chemical oxygen demand (COD), volatile fatty acids (VFAs), and reducing sugar were carried out.

2 Materials and Methods
2.1 Raw Materials
The anaerobic sludge used in the experiment was obtained from the Harbin Wenchang Sewage Treatment Plant, Harbin, China. It had been aeration cultured for 2 weeks, according to the ratio of 300:5:1 plus glucose, NH_4Cl, KH_2PO_4, with the sludge in brown color and a good settling for experiment [13]. The *Enteromorpha* used in the experiment was from the freshwater algae and acquired from the Institute of Hydrobiology of The Chinese Academy of Science, Wuhan, China. It had been air-dried in the Drying oven, and sealed with a breathable film in the bottle.

2.2 Optimisation of process parameters using RSM and experimental design
Batch experiments were conducted to analyze the effect at different MW power (400-800 W), pretreatment time (2-6 min) and liquid-solid ratio (20:1-60:1). The *Enteromorpha* powder was mixed with deionized water to make the desired liquid-solid ratio. All the experiments were conducted in triplicate [14].

A three-factor central composite design (CCD) was used to design the experiment for constructing models using design expert software version 8.0.6. Cumulative biogas production was chosen as the response variable, while MW power (A), pretreatment time (B) and liquid-solid ratio (C) were used as three independent variables, as is indicated in Table 1. The experimental design and corresponding experimental results are shown in Table 2. The results presented for COD, reducing sugar and carbohydrates are after pretreatment but before fermentation experiments. It shows difference between control and pretreatment.

2.3 Experimental Procedure
The MW pretreatment was carried out with a microwave oven in such a way that after every minute the microalgae solution was stirred and the temperature was measured with a thermometer. The temperature during pretreatment was recorded no higher than 50 °C. The anaerobic digestion of MW pretreated *Enteromorpha* with sludge was carried out batchwise. The experiment was divided

Table 1 Level of the independent variables for RSM.

Independent Variables	Parameters	Low Level	High Level
A	MW Power (W)	400	800
B	Pretreatment Time (min)	2	6
C	Liquid-Solid Ratio	20:1	60:1

Table 2 Experimental design for cumulative production and corresponding experimental results

Run	Power (W)	Time (min)	Ratio	COD (mg/L)	Reducing sugar (mg/L)	Carbonhydrate (mg/L)
1	800	2	40:1	3670	190	46
2	600	2	60:1	2320	462	34
3	400	4	20:1	3010	161	117
4	600	6	20:1	5750	471	150
5	600	4	40:1	5150	619	68
6	800	4	60:1	4690	263	121
7	400	2	40:1	3520	229	54
8	400	6	40:1	5370	293	107
9	600	6	60:1	4120	225	92
10	400	4	60:1	1500	165	43
11	800	4	20:1	5620	344	129
12	600	2	20:1	6320	308	108
13	800	6	40:1	8340	464	141

into four groups, each group contained 10 g MW pretreated *Enteromorpha* powder, and 30 ml of fresh sludge (TS: 5.9 g/L) in a 250 mL-scale glass bottle. The initial pH was adjusted at 7 by 1M NaOH and 1M HCl. The bottles were sealed with rubber stoppers and flushed with nitrogen gas for 5 min [15]. The digestion environment was maintained at 37 °C [16] and 150 rpm.

2.4 Analytical Methods
The measurements of soluble indexes including chemical oxygen demand (COD), pH, volatile fatty acids (VFAs) and reducing sugar were determined according to standard methods [17]. Biomass concentration like glucose concentration was estimated by 3,5-dinitrosalicylic acid (DNS) method using spectrophotometer (DR 3900, HACH, USA) at a maximum wavelength (λ_{max}) of 550 nm. The pH was recorded using a pH analyzer (PHS-3C, INESA, China). Volatile fatty acids (VFA) were analyzed using High-performance liquid chromatography (HPLC 7820A, Agilent Technologies, USA). The hydrogen content of the biogas was analyzed by gas chromatography (SP-2100A, BFRL, USA) with Thermal Conductivity Detector-Flame Ionization Detector (TCD-FID).

3 Results and Discussion
3.1 Effect of MW Pretreatment on COD and Reducing Sugar
The result of MW pretreatment on COD is shown in Fig. 2 (a). It is clearly shown that the group of liquid-solid ratio 20:1 provided the peak initial COD concentration value of 5,130 mg/L and the group 60:1, provided the least amount of value, i.e, 1,980 mg/L. The most significant increase in COD is found to be 1,605 mg/L and 1,985 mg/L obtained by the group 40:1 ratio at the MW power of 400W and 800W, respectively.

The change of reducing sugar concentration during the MW pretreatment is shown in Fig. 2 (b). The increase in reducing sugar with the groups of ratio 20:1 and 60:1 is not so significant. In contrast, the group with ratio 40:1 showed better performance on reducing sugar change. The highest amount of reducing sugar is found to be 0.0502 g/L. However, the group of MW power with 600 W indicated small increase and reached only 0.0062 g/L of reducing
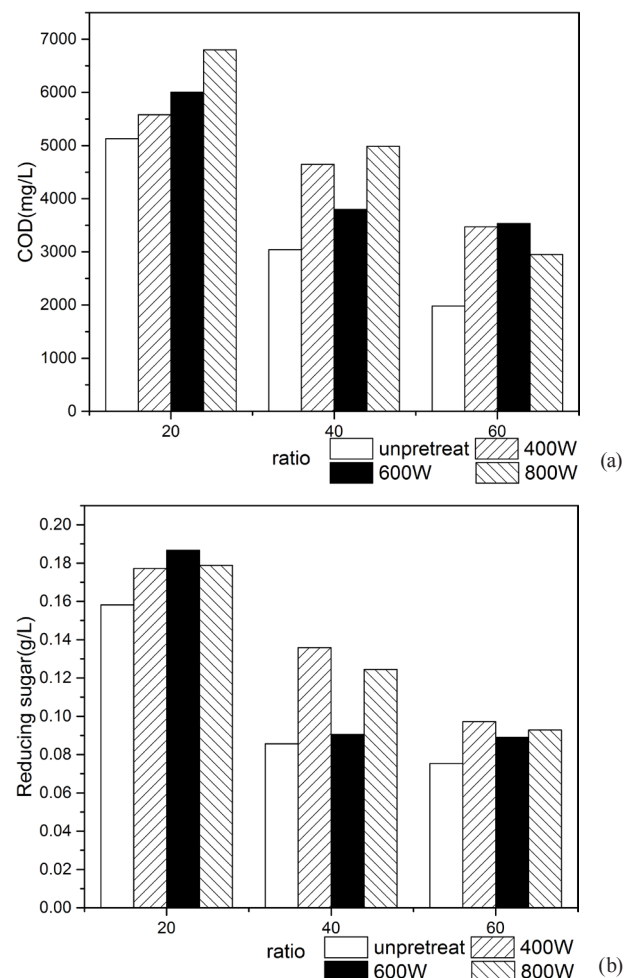
Fig. 2 (a) COD change with MW pretreatment (b) Reducing sugar change with MW pretreatment

sugar value. The behavior at 600 W is found to be similar for both COD and reducing sugar.

3.2 Optimisation of MW Pretreatment Process Parameters

The following regression equation (Eq. (1)) fits the experimental data of cumulative biogas production:

$$R\ sugar = 618.69 + 51.63A + 33.12B - 21.28C \\ -52.79AB - 21.31AC - 99.95BC \hspace{1cm} (1) \\ -229.11A^2 - 95.64B^2 - 156.32C^2.$$

The ANOVA result for the quadratic model is presented in Table 3. The determination of coefficient R^2 and adjusted R^2 were found to be 0.9009 and 0.6036, respectively. The ANOVA calculation shows that the P-value (Prob > F) is 0.0560, which means the relationship between the independent variables and the response values investigated in this experiment are significant and the scheme is reliable. From the impact of different factors in this experiment on the biogas production, the term A^2 Prob > F value of ratio is 0.0303 which is less than 0.05, meaning that A^2 had significant influence in the biogas production. The term C^2 also has conspicuous effect on biogas production. Further, comparing the P-value with A, B and C, it can be found that the influence of these 3 factors was MW power > pretreatment time > liquid-solid ratio.

The response surface design results in the form of three-dimensional response curves are shown in Fig. 3.

Table 3 ANOVA of the quadratic regression model for cumulative biogas production

Source model	Sum of squares	Df (degree of freedom)	Mean square	F value	P-value Prob > F
Model	10173.23	9	2414.62	10.03	0.0560
A-power	21327.53	1	21327.53	2.68	0.2004
B-time	8774.55	1	8774.55	1.10	0.3711
C-ratio	3621.52	1	3621.52	0.45	0.5485
AB	11146.29	1	11146.29	1.40	0.3221
AC	1816.21	1	1816.21	0.23	0.6657
BC	39958.81	1	39958.81	5.01	0.1110
A^2	12005.48	1	4205.05	15.06	0.0303
B^2	20909.20	1	20909.20	2.62	0.2037
C^2	55852.15	1	5852.15	15.01	0.0372
Residual	23904.85	3	7968.28		
Cor Total	2.412E+005	12			

$R^2 = 0.9009$, adjusted $R^2 = 0.6036$

It can be observed that the curvature of MW power is slightly larger than the pretreatment time, indicating that the effect of MW power on the biogas production is significantly larger than the pretreatment time. The same observation can also depict the plot of liquid-solid ratio and MW power. The curvature of MW power is slightly larger than liquid-solid ratio. In the plot of liquid-solid ratio and pretreatment time the curvature of liquid-solid ratio is less than pretreatment time, indicating that pretreatment time is a more effective factor. In contour plots, it is found that the contour line is an obvious oval, which indicates that the interaction between both the two factors are significant. This is in continuity with the variance analysis. The elliptical contour plots show the good interaction between the independent variables. The optimum conditions for the MW pretreatment are found to be, MW power at 656.92 W, pretreatment time at 5.10 min and liquid-solid ratio at 33.63:1.

3.3 Biogas Production

MW pretreatment power of 600 W is used to perform the anaerobic digestion experiment to observe the real effect on biogas yield with different liquid-solid ratio and time. The biogas production influenced by different MW pretreatment conditions is shown in Fig. 4. The gas amount increased to 238, 223, 244 and 188 mL for the groups 20:1, 2 min, 40:1, 4 min, 20:1, 6 min and control, respectively. The two groups 20:1, 6 min and 20:1 2 min provide maximum gas production amount of 244 mL and 238 mL, respectively. The group with liquid-solid ratio 40:1 and pretreatment time of 4 min showed an abrupt increase with 36 mL at 60 h as compared to control. The maximum cumulative biogas and the amount of hydrogen produced during the experiment are presented in Table 4.

The biogas production potential of carbohydrate is much higher than that of lipid and protein. The different carbohydrate content could be one of the reasons for different biogas production [18]. It can be observed form Fig. 2 (b) that the reducing sugar value increased after MW pretreatment indicating that pretreatment dissolute the *Enteromorpha* cell wall and releases more carbohydrate and increases biogas production.

3.4 Change in COD and reducing sugar concentration

The dynamic change of COD during anaerobic digestion process is shown in Fig. 5. It is found that the liquid-solid ratio in 20:1 displays good performance, especially the group of ratio 20:1 and 6 min in 600 W achieves highest
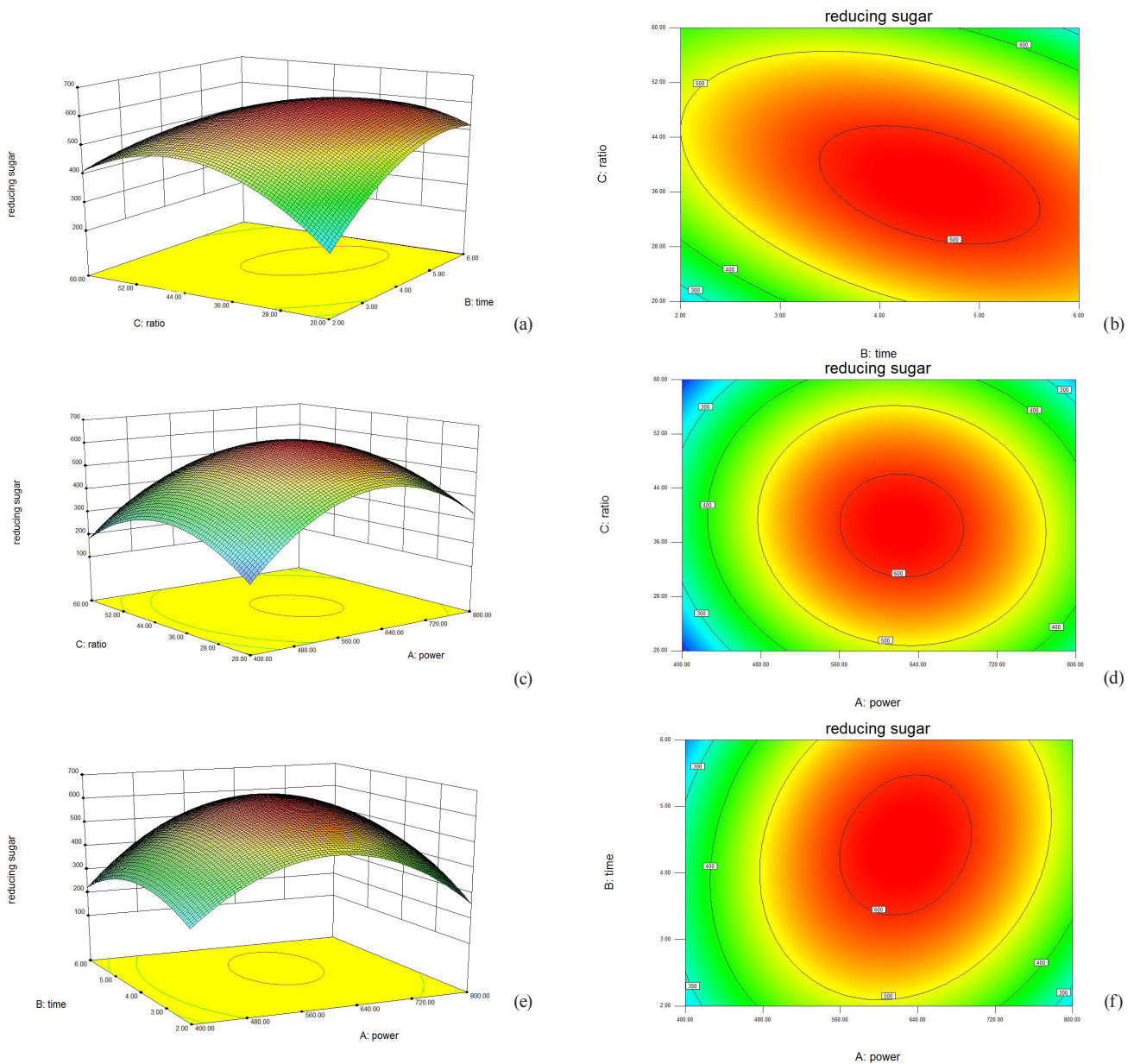
Fig. 3 (a-f) Response surface plot and Contour plots for biogas

COD value of 10,420 mg/L. However, the groups of liquid-solid ratio 60:1 and 2 min presents a low value. Fig. 6 shows the effect for reducing sugar during anaerobic digestion. It is found that the ratio 40:1, 4 min group provides highest value of 0.79 g/L and provides less biogas yield. Low reducing sugar value with high gas production means that the most reducing sugar had been used to produce the gas in this period. The highest biogas amount with more sugar consumption during anaerobic digestion process is achieved by group 20:1, 6 min.

3.5 VFA production during fermentation

The production of VFA amount measured during the experiment is shown in Fig. 7. It is found that the amount of butyric acid had a very significant change in two groups. The amount of increase can reach 2,808 mg/L and 2,644 mg/L in group of 20:1 liquid-solid ratio, 6 min and 20:1 liquid-solid ratio, 2 min, respectively. High biogas yield is observed with high acetic acid and butyric
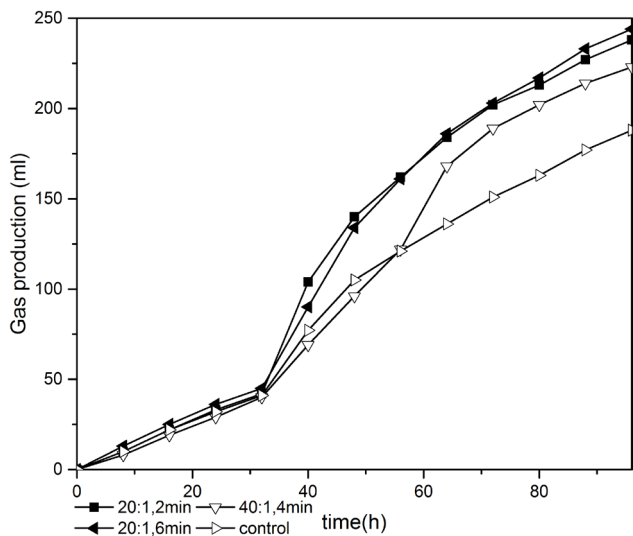
Table 4 Cumulative biogas production and amount of hydrogen produced during the experiment

	Control	20:1 2min	40:1 4min	20:1 6min
Cumulative Biogas (ml)	188	238	223	244
Hydrogen % (v/v)	17.53	49.51	35.64	45.11

Fig. 4 Biogas production influenced by different MW pretreatment condition
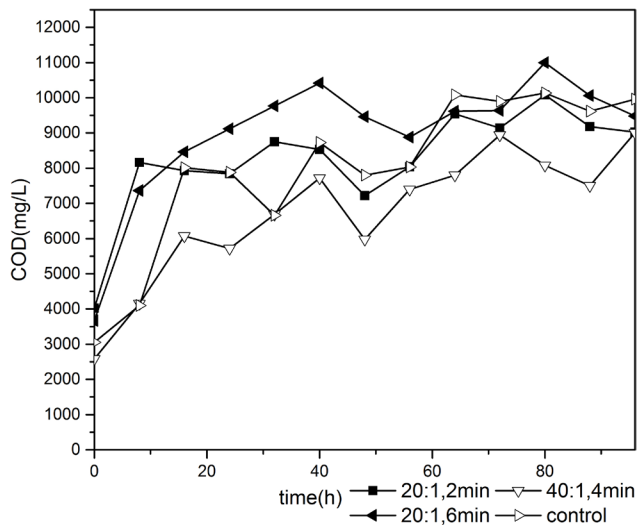

Fig. 5 Dynamic change of COD during anaerobic digestion
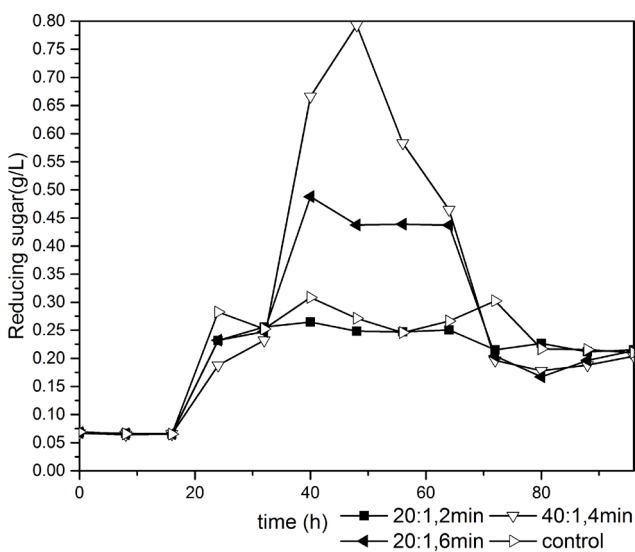

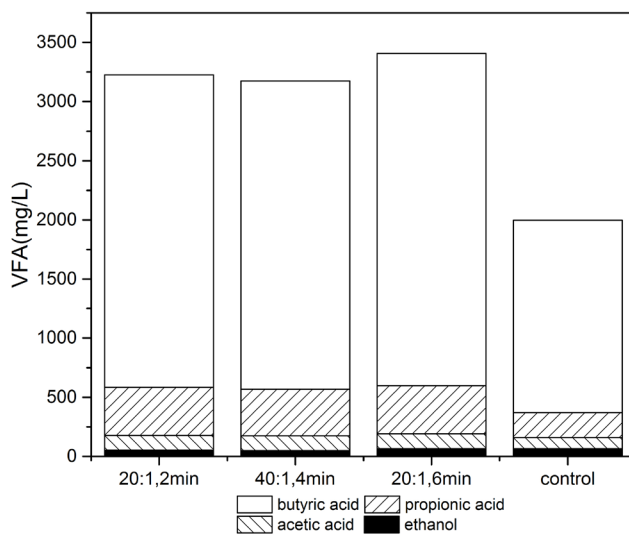**Fig. 6** Dynamic change of reducing sugar during fermentation

Fig. 7 VFA production affected by different MW pretreatment conditions

Table 5 Biogas potentials of pretreated microalgae

Pretreatment method	Algae	Pretreatment condition	Biogas yields after pretreatment	Ref.
Beating	*Pelvetia caniculata*	Hollander beater	444.3 mL biogas/g TS	[20]
Ultrasound	*Hydrodictyon reticulatum*	20 kHz 40 J/mL	Methane production 2.3 times higher	[21]
Thermal	*Scenedesmus*	80 °C	57 % methane yield increase	[22]
Chemical	*Chlorella vulgaris*	4 M NaOH	237.9 mL CH4/g COD	[23]
	Nannochloropis salina	5 times until boiling at 600 W	Biogas yield increase of 40 %	[24]
Microwave	Micro-algal from a high rate algal ponds	65.4 MJ/kg TS	Biogas yield increase of 78 %	[25]
	Enteromorpha	Shown above	24.4 mL biogas/g dry algae	This study

acid production. In contrast, it had a low level ethanol amount, and it is found that ethanol accumulation negatively affects the biogas yield, since ethanol production has no contribution to biogas production [19]. The Table 5 listed the biogas potentials between different pretreatment of microalgae.

4 Conclusions

The MW pretreatment enhanced the biogas production by providing highest amount of biogas yield with 244 mL, amount of COD with 10,420 mg/L and a highest amount of increase of reducing sugar from 0.24 g/L to 0.79 g/L. The best conditions of *Enteromorpha* MW pretreatment are: MW

power 656.92 W, pretreatment time 5.10 min, liquid-solid ratio 33.63:1. The presented results demonstrate the practicability of RSM optimum strategy and show the robustness of MW pretreatment with anaerobic digestion of microalgae (*Enteromorpha*) for enhancement in biogas yield.

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